#### 2019 Sep-Tek Exam problems

### Problem 3: Distillation (30%)

A mixture of 35 mol% benzene and 65 mol% toluene is separated in a distillation tower at atmospheric conditions. The feed is a saturated liquid. The feed flow is 100 kmol/h. The distillate should be 95 mol% benzene (with a total condenser), while the bottom product (liquid) should be 90 mol% of toluene. The x-y diagram of the benzene-toluene system is given in the attachment 1. Please:

- a) Draw a process flow diagram including the product flows (D, B) and internal flows (L<sub>T</sub>, V<sub>T</sub>, L<sub>B</sub>, V<sub>B</sub>). (3%)
- b) Determine D and B in the process. (3%)
- c) Find graphically the minimum number of equilibrium stages (Nmin). (2%)
- d) Find the minimum reflux (Rmin). (4%)
- e) Use the McCabe–Thiele method to determine the number of equilibrium stages N and determine the optimal feed-stage location (R=1.4Rmin). (10%)
- f) Compute the required energy consumption ( $\Delta H_{Vap}$  for benzene and toluene are 34 kJ/mol and 38 kJ/mol, respectively). (8%)



Attachment 1. Equilibrium diagram of the benzene-toluene system at 1 atm.

### Solution 3:

a) The flow chart includes the condenser, reboiler and the flows (3 p)



b) Make material balance overall and component:

F=D+B=100 (1)

 $Fx_F = Dx_D + Bx_B \rightarrow 100 \times 0.35 = D \times 0.95 + B \times 0.1$  (2)

Combine (1) and (2)  $\rightarrow$  D= 29.4 [kmol/h]

B=70.6 [kmol/h] (3p)

c) Nmin (2p)



d) Determine Rmin

R=1.4×Rmin

Make the q-line: slope--> vertical

Find the cross point at the x-y curve (0.35, 0.55) (if the data are +/-0.02 is acceptable)

Slope =  $\text{Rmin}/(\text{Rmin}+1) = (0.95-0.55)/(0.95-0.35) \rightarrow \text{Rmin} = 2 (4p)$ 

(if the data are +/-0.1 is acceptable)



e) <u>Find the reflux</u>:

 $R=1.4 \times Rmin=2.8$  (if the data are +/-0.1 is acceptable) (2p)

Draw operating lines:

q-line (2p)

Top operating line:

Using slope = R/(R+1) = 2.8/3.8=0.737, draw a straight line starting from (0.95,0.95),

or connect this point with the intercept at y axis (0.25,0), where  $x = x_D/(R+1)$ 

=0.95/(1+2.8)=0.25 (**2p**)

Bottom operating line:

Connect (xB, xB) and cross of the top operating line at the q-line (2p)

Make the stairs: (2p).

N=11 No. 7 steps over the cross of the operating lines.

Thus, the feed stage is at No. 7 from the top, and the number of equilibrium stages N is 11 including the reboiler.



f)  $L_T=D\times R=29.4 \times 2.8 = 82.32 \text{ [kmol/h]}$  (1p)  $V_T=L_T+D= 82.32+29.4 = 111.72 \text{ [kmol/h]}$  (1p)  $L_B=L_T+F= 82.32+100=182.32 \text{ [kmol/h]}$  (1p)  $V_B=VT= 182.32 - 70.6=111.72 \text{ [kmol/h]}$  (1p) yB= 0.21 (xB=0.1 at x-y diagram)  $\Delta HBmix = 0.21\times 34+0.79\times 38=37.16 \text{ kJ/mol}$  (1p)  $\Delta HDmix = 0.95\times 34+0.05\times 38= 34.2 \text{ kJ/mol}$  (1p)  $Q_B = V_B \times \Delta HBvap = 111.72\times(1000/3600) \times \Delta HBmix \text{ J/s}$ (still 2p if the  $\Delta HBvap$  data were the data for pure toluene, = 1153.2 kJ/s = 1.15 MW) (1p)

 $Qc = V_T \cdot \Delta HDvap = 111.72 \times (1000/3600) \times \Delta HDmix \times 1000 \text{ J/s}$ 

(still 2p if the  $\Delta$ HBvap data were the data for pure benzene

1061.34 J/s = 1.06 (MW) (1p)

## Problem 4: Absorption (10%)

A membrane contactor is used to absorb a small amount of A from a mixture of A+B (assume 2 mol% A in B), in which 98% of A is required to be absorbed. The feed gas flow is 300 kmol/h, at 30°C, 1atm. Clean water (L=250 kmol/h) is used as the absorbent in a countercurrent flow. The gas-liquid equilibrium relationship for the A in water can be described by y=0.6x at 30°C, 1atm.



- a) Calculate the molar flows and compositions of the gas and liquid outlets. (4%)
- b) Determine the minimum flow of the liquid (Lmin). (4%)
- c) State the advantages and disadvantages of using membrane contactor as an absorber. (4%)

#### Solution 4: Reasonable errors in calculation are acceptable.

a) Determine the unknown parameters in the flow sheet. (V1, y1),  $(L_1)$  and  $(x_1)$ . (4p)

Known: 
$$y_0=0.02$$
,  $x_0=0$ ,  $V_0=300$ ,  $L_0=250 = L'$   
So:  $V'=V_0(1-y0) = 300 \times 0.98 = 294$  kmol/h  
A inlet  $=V0$  ( $y_0$ )  $= 300 \times 0.02 = 6$  kmol/h  
A outlet  $= (1-0.98) \times A$  inlet  $= 0.12$  kmol/h  
 $V1=V'+Aoutlet = 294+0.12 = 294.12$  kmol/h  
 $y1=A$  outlet/ $V1 = 0.12/(294.12) = 0.00041$   
A absorbed:  $La=0.98 \times A$  inlet  $= 5.88$   
 $L_1=L'+La = 250+5.88 = 255.88$   
 $X_1=La/L_1 = 5.88/250 = 0.0235$ 

b) Minimum flow of the liquid  $L_{min}$  (4p)

 $L_{min}(x^{*}_{1}) - Lmin'x0 = 0.98 \times y_{0} V_{0}$   $x^{*}_{1} = y_{0}/0.6 = 0.02/0.6 = 0.0333$   $L_{min} = 0.02 \times 0.98 \times 300/(0.02/0.6) = 176.4 \underline{kmol/h}$   $Lmin' = \underline{Lmin(1-x^{*})} = 170.52 \underline{kmol/h}$ 

Or by using the operating line method.

c) <u>Advantages:(4p)</u>

# (4p for all, but 1p for each point given)

- Non-dispersive contact (no flooding, foaming or entrainment),
- High interfacial area
- Solvent hold up can be low
- Predictable performance
- Easy, linear scaling-up

# Disadvantages:

- Extra mass transfer resistance from the membrane
- Membrane long term stability issue
- Sensitive pressure control: wetting/bubbling/solvent evaporation