

Oving 8

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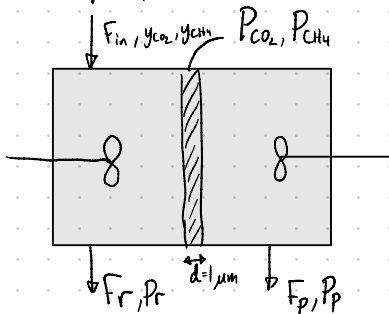
Separate a feed gas that consists of CO₂ and methane with a cellulose acetate membrane that has effective membrane layer thickness of 1 μm. The feed gas flow rate is 1 mol/s and has 50 mol % of CO₂ and 50 mol % of methane at 35 °C. The membrane permeabilities were measured at 35°C:

$P_{CO_2} = 15.0 \times 10^{-10}$ [cc(STP)cm]/[cm² s cm Hg] and $P_{CH_4} = 0.48 \times 10^{-10}$ [cc(STP)cm]/[cm² s cm Hg]. A completely mixed membrane module is used with retentate side pressure $p_r = 20$ atm and permeate side pressure $p_p = 1.1$ atm.

- Determine the permeate and retentate purity for stage cuts: 0.25, 0.5, 0.75.
- Evaluate the fluxes and the membrane area
- Find the limit for maximum permeate purity

Note: You may use a numerical (Excel, Matlab), graphical or analytical solution.

Formler er hentet fra powerpoints:



La $A = CO_2$

a) Operating line: $y_r = \frac{y_A - \theta y_{Ap}}{1 - \theta}$

Rate transfer: $y_{Ar} = \frac{y_{Ap} [R(1 - y_{Ap})(\alpha - 1) + 1]}{\alpha - (\alpha - 1)y_{Ap}}$

$$R = \frac{P_p}{P_r} = \frac{1.1}{20} = 0.055$$

$$\alpha = \frac{P_A}{P_{CH_4}} = \frac{15}{0.48} = 31.25$$

```
import scipy.optimize as sco
import numpy as np
# Konstante
R = 1./20
theta = 0.5
thetas = np.array([0, 0.25, 0.5, 0.75, 1])
P_A = 15e-10
P_B = 0.48e-10
alpha = P_A/P_B
L = 1
delta = 1e-6
rho_A = 1.1
rho_B = 1./22400

def operating_line(y_ap):
    y_ar = (y_ap - stage_cut*y_ap) / (1 - stage_cut)
    return y_ar

def rate_transfer(y_ap):
    y_ar = (y_ap*(R*(1-y_ap)*(alpha-1)+1)) / (alpha - (alpha-1)*y_ap)
    return y_ar

def solve(y_ap):
    return rate_transfer(y_ap) - operating_line(y_ap)
print("=====")
for stage_cut in thetas:
    if stage_cut == 1:
        y_ap = yA
    else:
        ans = sco.root(solve, 0.9)
        y_ap = ans[0]
        y_ar = rate_transfer(y_ap)
        print(f"for theta = {stage_cut}:")
        print(f"y_ar = {y_ar:.4f} og y_ap = {y_ap:.4f}")
        J_AW = 76/(18e-4) * P_A * (y_ar - y_ap) - 2*P_B*y_ap
        J_BW = 76/(18e-4) * P_B * (y_ar - y_ap) - 2*P_A*(1 - y_ap)
        print(f"J_AW = {J_AW:.5f} og J_BW = {J_BW:.5f}")
        A = (cf * stage_cut + y_ap)/(J_AW + rho_A) + 18e-4/6
        print(f"A = {A:.2f}")
        print("=====")
```

Setter inn i python, løser med scipy.optimize.root

⇒ $\theta = 0.25$, $y_{Ar} = 0.3545$, $y_{Ap} = 0.9365$
 $\theta = 0.50$, $y_{Ar} = 0.1718$, $y_{Ap} = 0.8282$
 $\theta = 0.75$, $y_{Ar} = 0.0856$, $y_{Ap} = 0.6381$

$$b) J_{AV} = \frac{P_A}{L} (P_r y_{Ar} - P_p y_{Ap})$$

$$J_{BV} = \frac{P_B}{L} (P_r (1 - y_{Ar}) - P_p (1 - y_{Ap}))$$

enheter: $\frac{(\text{cc (STP) cm}) / (\text{cm}^2 \cdot \text{s cmHg})}{\mu\text{m}} \cdot \text{atm}$

$\frac{(\text{cc (STP) cm}) / (\text{cm}^2 \cdot \text{s cmHg})}{\text{atm} \cdot 10^{-4} \frac{\text{cm}}{\text{atm}}} \cdot \text{atm} \cdot \frac{76 \text{ cmHg}}{\text{atm}}$

Løser direkte i python

$$\Rightarrow \Theta = 0,25, J_{AV} = 0,00691, J_{BV} = 0,000468$$

$$\Theta = 0,50, J_{AV} = 0,00288, J_{BV} = 0,000597$$

$$\Theta = 0,75, J_{AV} = 0,00115, J_{BV} = 0,000653$$

$$\frac{76}{10^{-4}} \cdot \frac{\text{cc (STP)}}{\text{cm}^2 \cdot \text{s}}$$

↑
korreterer med

Finner arealen ved:

$$J_{An} = J_{Av} J_{AV}, J_{An} = \frac{\dot{N}_{Ap}}{A} = \frac{\dot{N}_p y_{Ap}}{A} = \frac{\dot{N}_r \Theta \cdot y_{Ar}}{A}$$

$$\Rightarrow A = \frac{\dot{N}_r \cdot \Theta \cdot y_{Ar}}{J_{AV} \cdot J_{AV}} = \left[\frac{\text{mol/s}}{\frac{\text{cc (STP)}}{\text{cm}^2 \cdot \text{s}}} \right] [\text{?}] = [\text{cm}^2]$$

J_{AV} er gitt i: $\frac{\text{mol}}{\text{cc STP}}$ Må finne J_{AV} med enheter $\frac{\text{mol}}{\text{cc STP}}$
Se siste side

$$\Rightarrow J_{AV} = \frac{1 \text{ mol}}{22400 \text{ cc STP}}$$

Løser i python:

$$\Theta = 0,25, A = 75,9 \text{ m}^2$$

$$\Theta = 0,50, A = 322 \text{ m}^2$$

$$\Theta = 0,75, A = 931 \text{ m}^2$$

c) Dette er når $\Theta = 0$, da er operating line vertikal,

Fra python, er da:

$$\Theta = 0, y_{Ap, \text{max}} = 0,9656$$

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A cellulose-acetate membrane with an area of $4.0 \times 10^{-3} \text{ m}^2$ is used at 25°C to determine the permeability constants for reverse osmosis of a feed salt solution containing 12.0 kg NaCl/m^3 ($\rho = 1005.5 \text{ kg/m}^3$). The product solution has a concentration of $0.468 \text{ kg NaCl/m}^3$ ($\rho = 997.3 \text{ kg/m}^3$). The measured product flow rate is $3.84 \times 10^{-8} \text{ m}^3/\text{s}$ and the pressure difference used is 56.0 atm . Calculate the permeance constant and the solute rejection R . (Geankoplis, 4th ed.)

Osmotic Pressure of Various Aqueous Solutions at 25°C .

Sodium Chloride Solutions			Sea Salt Solutions		Sucrose Solutions	
$\frac{\text{mol NaCl}}{\text{kg H}_2\text{O}}$	Density (kg/m^3)	Osmotic Pressure (atm)	Wt. % Salts	Osmotic Pressure (atm)	Solute Mol. Frac. $\times 10^{-3}$	Osmotic Pressure (atm)
0	997.0	0	0	0	0	0
0.01	997.4	0.47	1.00	7.10	1.798	2.48
0.10	1001.1	4.56	3.45	25.02	5.375	7.48
0.50	1017.2	22.55	7.50	58.43	10.69	15.31
1.00	1036.2	45.80	10.00	82.12	17.70	26.33
2.00	1072	96.2				

$$\Delta p = 56 \text{ atm}, \quad \dot{V}_p = 3.84 \cdot 10^{-8} \text{ m}^3/\text{s}, \quad A = 4 \cdot 10^{-3} \text{ m}^2$$

$$C_F = 12.0 \text{ kg/m}^3, \quad C_P = 0.468 \text{ kg/m}^3$$

$$\rho_F = 1005.5 \text{ kg/m}^3, \quad \rho_P = 997.3 \text{ kg/m}^3$$

Produktstrømmen er fortynnet, antas $\rho_w = \rho_P = 997.3 \text{ kg/m}^3$

Finner fluksen av vann og salt fra produktstrømmen

$$N_w = \frac{\dot{V}_p \cdot \rho_w}{A} = \frac{3.84 \cdot 10^{-8} \text{ m}^3/\text{s} \cdot 997.3 \text{ kg/m}^3}{4 \cdot 10^{-3} \text{ m}^2} = 9.57 \cdot 10^{-3} \frac{\text{kg}}{\text{m}^2 \cdot \text{s}}$$

$$S = \text{salt} \quad N_s = \frac{\dot{V}_p \cdot C_P}{A} = \frac{3.84 \cdot 10^{-8} \text{ m}^3/\text{s} \cdot 0.468 \text{ kg/m}^3}{4 \cdot 10^{-3} \text{ m}^2} = 4.49 \cdot 10^{-6} \frac{\text{kg}}{\text{m}^2 \cdot \text{s}}$$

$$\text{Feed: } m_{\text{NaCl}} = 12 \text{ kg/m}^3$$

$$m_w = (1005.5 - 12) \text{ kg/m}^3 = 993.5 \text{ kg/m}^3$$

$$\frac{n_{\text{NaCl}}}{m_w} = \frac{\left(\frac{12 \text{ kg/m}^3}{58.44 \text{ g/mol}} \right)}{993.5 \text{ kg/m}^3} = 0.2067 \text{ mol NaCl / kg H}_2\text{O}$$

Ønsket π_F , interpoleres i tabellen

$$a = \frac{22,55 - 4,56}{0,5 - 0,1} = 44,975$$

$$y - 4,56 = 44,975(x - 0,1)$$

$$\text{L.e. } x = 0,2067$$

$$\Rightarrow \pi_F = y = 4,56 + 44,975(0,2067 - 0,1) = \underline{9,36 \text{ atm}}$$

For produktstrømmen

$$m_{\text{NaCl}} = 0,468 \text{ kg/m}^3$$

$$m_w = (998,3 - 0,468) \text{ kg/m}^3 = 996,832 \text{ kg/m}^3$$

$$\frac{n_{\text{NaCl}}}{m_w} = \frac{\left(\frac{0,468 \text{ kg/m}^3}{58,44 \text{ g/mol}} \right)}{996,832 \text{ kg/m}^3} = \underline{8,034 \cdot 10^{-3} \text{ mol NaCl / kg H}_2\text{O}}$$

$$\text{Interpoleres igen: } \Rightarrow \pi_p = \underline{0,38 \text{ atm}}$$

$$\Delta \pi = 9,36 - 0,38 = 8,98 \text{ atm}$$

$$a_w = \frac{N_w}{\Delta p - \Delta \pi} = \frac{9,57 \cdot 10^{-3} \frac{\text{kg}}{\text{m}^2 \cdot \text{s}}}{(56 - 8,98) \text{ atm}} = \underline{\underline{2,04 \cdot 10^{-4} \frac{\text{kg}}{\text{m}^2 \cdot \text{s} \cdot \text{atm}}}}$$

$$a_s = \frac{N_s}{\Delta c} = \frac{4,49 \cdot 10^{-6} \frac{\text{kg}}{\text{m}^2 \cdot \text{s}}}{12 \frac{\text{kg}}{\text{m}^3} - 0,468 \frac{\text{kg}}{\text{m}^3}} = \underline{\underline{3,89 \cdot 10^{-7} \text{ m/s}}}$$

$$\underline{\underline{R = 1 - \frac{C_p}{C_F} = 1 - \frac{0,468}{12} = 0,961}}$$

Appendix

ρ_{AV} . Er molar tetthet $\Rightarrow \frac{n}{V}$, hvor vi dette tilfellet trenger enheten
cc STP for volumet

Dermed har vi: $\rho_{AV} = \frac{n}{V}$

Bruker vi ideell gasslov, så blir: $pV = nRT \Rightarrow \frac{n}{V} = \frac{p}{RT}$

Siden cc STP = cm^3 ved STP, så setter vi inn STP i uttrykket:

$$\rho_{AV} = \frac{n}{V} = \frac{1 \text{ mol}}{0.0821 \frac{\text{atm} \cdot \text{L}}{\text{mol} \cdot \text{K}} \cdot 273 \text{ K}} \approx \frac{1}{22.4 \text{ L/mol}}$$

Før de som ikke kjenner igjen dette tallet, så er det molare volumet til gass ved STP, $V_m = \frac{V}{n} = 22.4 \text{ L/mol}$

Per definisjon, siden $\rho_{AV} = \frac{n}{V}$ og $V_m = \frac{V}{n} \Rightarrow \rho_{AV} = \frac{1}{V_m}$

(Men det trengs ikke i oppgaven)

Men vi mangler fortsatt å få cc STP enheten, siden vi fant ρ_{AV} ved STP, så er:

$$\rho_{AV} = \frac{1}{22.4 \text{ L/mol}} \text{ (ved STP)} = \frac{1 \text{ mol}}{22.4 \text{ L STP}}$$

Litt enhetskonvertering:

$$1 \text{ cc STP} = 1 \text{ cm}^3 \text{ STP}$$

$$1 \text{ cm}^3 \text{ STP} = 10^{-3} \text{ dm}^3 \text{ STP}$$

$$1 \text{ dm}^3 \text{ STP} = 1 \text{ L STP}$$

$$\left. \begin{array}{l} 1 \text{ cc STP} = 1 \text{ cm}^3 \text{ STP} \\ 1 \text{ cm}^3 \text{ STP} = 10^{-3} \text{ dm}^3 \text{ STP} \\ 1 \text{ dm}^3 \text{ STP} = 1 \text{ L STP} \end{array} \right\} \Rightarrow 1 \text{ L STP} = 1 \text{ L STP} \cdot \frac{1 \text{ dm}^3 \text{ STP}}{1 \text{ L STP}} \cdot \frac{10^3 \text{ cm}^3 \text{ STP}}{1 \text{ dm}^3 \text{ STP}} \cdot \frac{1 \text{ cc STP}}{1 \text{ cm}^3 \text{ STP}} \\ \Rightarrow 1 \text{ L STP} = 1000 \text{ cc STP}$$

Dermed:

$$\rho_{AV} = \frac{1 \text{ mol}}{22.4 \text{ L STP}} = \frac{1 \text{ mol}}{22400 \text{ cc STP}}$$